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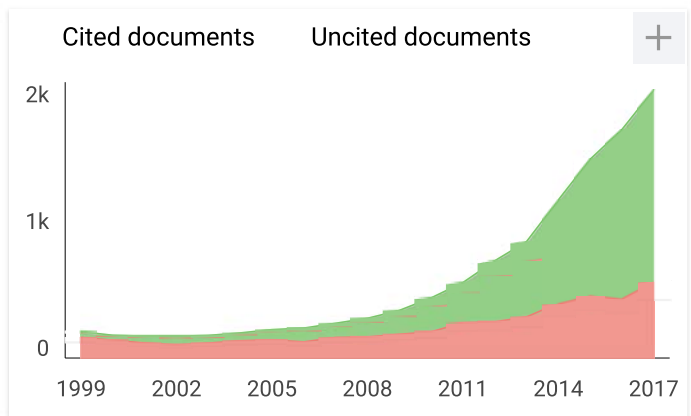
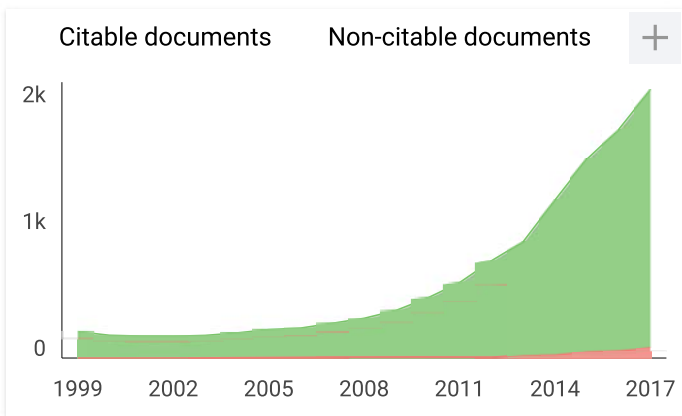
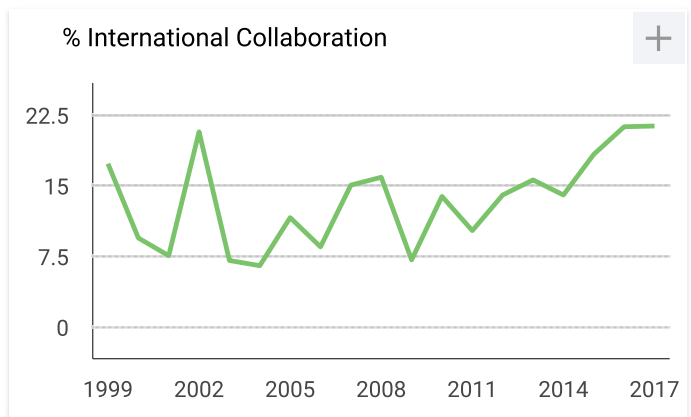
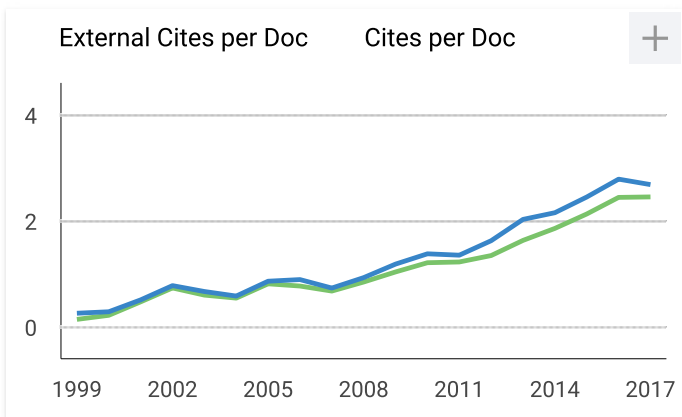
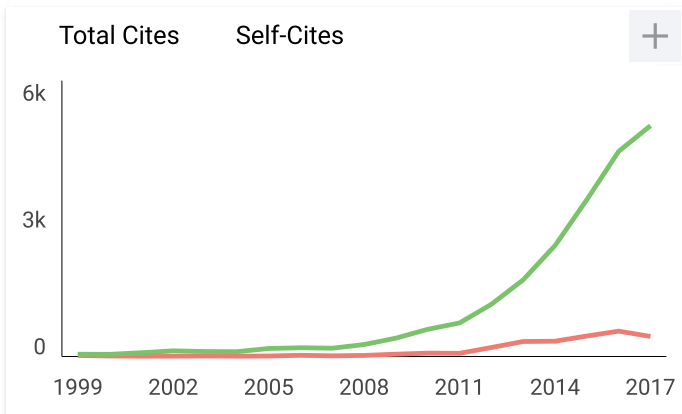
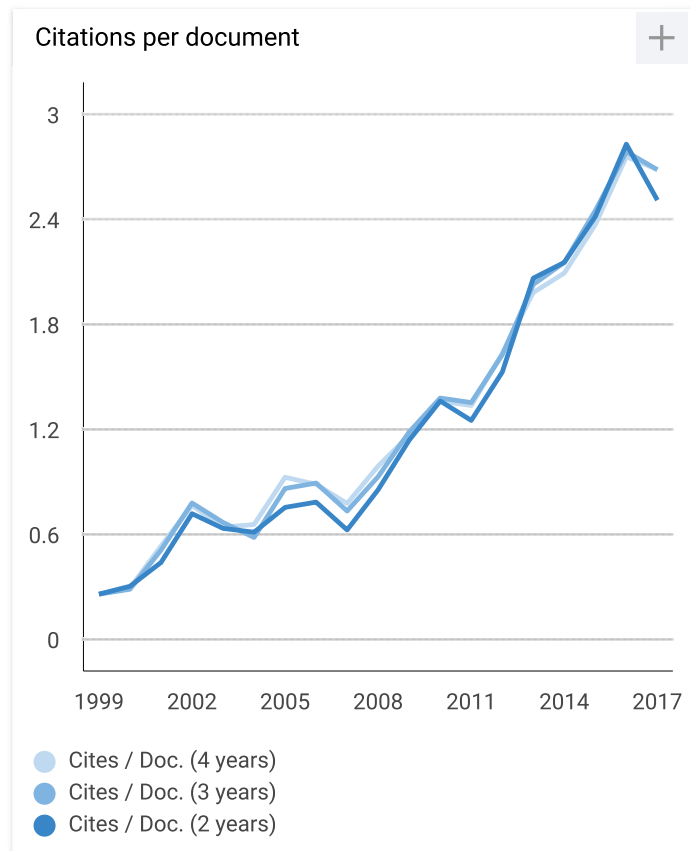
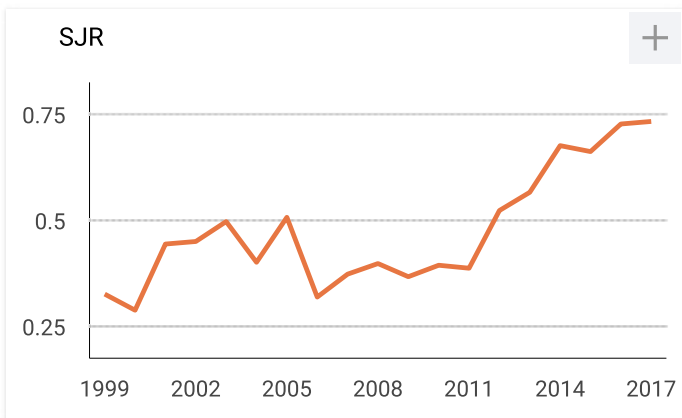
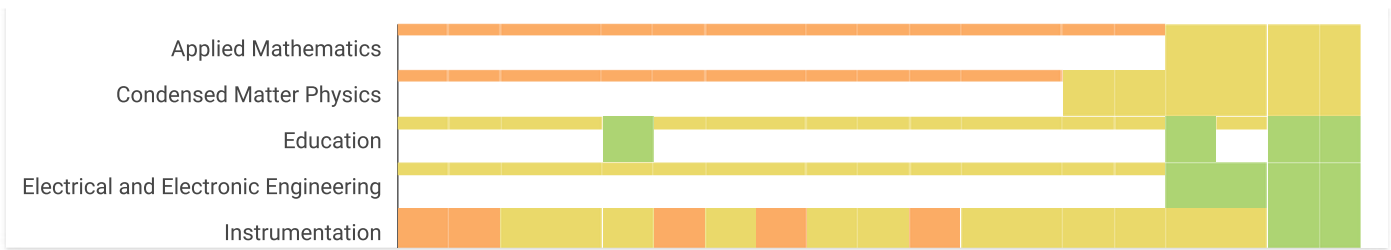
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# Liquid level sensor using fiber bundle

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## ARTICLE INFO

### Keywords:

Liquid level sensor  
Fiber bundle  
Displacement sensor

## ABSTRACT

Liquid level sensors can be constructed using a pair of bundle probe based on fiber-optic displacement sensor. The working mechanism of the sensor is detecting displacement in the reflector which is attached to membrane (reflector displacement device or RDD) due to changes in the level of the liquid. Displacement of reflector is detected through changes in the intensity of reflected light from reflector into an optical fiber that serves as the recipient of the light. Other optical fiber acts as a transmitter of light. Three types of RDD was used in this experiment, namely RDD consisting of 1, 2, and 3 layers of the membrane. The best performance is shown by the sensor using RDD with 1 layer membrane. Sensor range, linear region, sensitivity, and resolution sensor generated each of 115 cm, 110 cm, 0.37 mV/cm, and 1.45 cm.

## 1. Introduction

Application of optical fiber as sensor can be based on the modulation of the intensity, wavelength, and phase. Application of optical fiber liquid level sensor has been done mostly based on the modulation of the intensity and wavelength. Optical fiber liquid level sensors based on wavelength modulation can use fiber Bragg grating [1], tapered chirped [2], and long period [3] which is connected with a buoy. The use of fiber optic interferometry with two photonic crystal fiber (PCF) that is placed on a trajectory of optical properties [4] has also been done. Sensor range for sensor based on wavelength modulation is not too wide (the order of mm), but the resolution is good. For liquid level sensors with a wider range, intensity modulation is more likely to be used. Some examples of Optical fiber liquid level sensors based modulation intensity are using fiber optic connected with cone-shaped transparent elements [5], prism [6–8], and plastic optical fiber at its polished cladding [9] which acts as a sensor probe. The liquid level is detected when the sensor probe interacts with the liquid. Such interactions cause a change in the total reflected light intensity in the probe. Fiber coupler that has been used to detect the level of liquid (gasoline) is based on displacement sensor [10]. The sensing principle is to detect displacement of reflector, which is attached to the membrane (reflector displacement device), due to the change of liquid hydrostatic pressure. The displacement of reflector can be detected using fiber coupler from the change of optical power light reflected by the reflector. Liquid level sensors of this type have been developed until two levels so that the working area (linear region) doubled [11]. Other methods to detect liquid level are opto-fluidic techniques [12] and the transmission of

optical signals on the surface of liquids [13]. Opto-fluidic technique is conducted through observation of a beam spot size of reflected surface of liquid. The optical signal broadcasting technique is carried out through an optical fiber and other optical fiber that serves as the receiver of the reflected signal from the surface of the liquid. Signals emitted or received by optical fiber is focused by a lens.

A pair bundle probe (fiber bundles consist of a pair) has been successfully to be used as a displacement sensor based on modulation of intensity. Displacement of reflector (mirror) detected through changes in the intensity of reflected light from the reflector go into one fiber that acts as the recipient of the beam of light, while other fiber serves as a transmitter of light to the reflector [14]. Based on working principle of liquid level sensor using fiber coupler as well as consider the ability of a pair bundle probes to detect displacement of reflector, then in this paper will be reported liquid level sensor that is constructed using a pair bundle probe.

## 2. Sensors design and operating principle

The working mechanism of liquid level sensor can be explained based on the schematic diagram of the sensor as shown in Fig. 1(a). The components of the sensor consist of a laser as light source, optical detectors, a pair bundle probes (each fiber serves as a transmitter and receiver light), and the tank as a container of liquid. At the base of the tank, there is a reflector displacement device (RDD), as shown in Fig. 1(b). RDD comprises a reflector (flat plate) which is glued together on the membrane. Reflectors will shift ( $z'$ ) if the hydrostatic pressure changes ( $P_h$ ) due to a change in the liquid level ( $h$ ).

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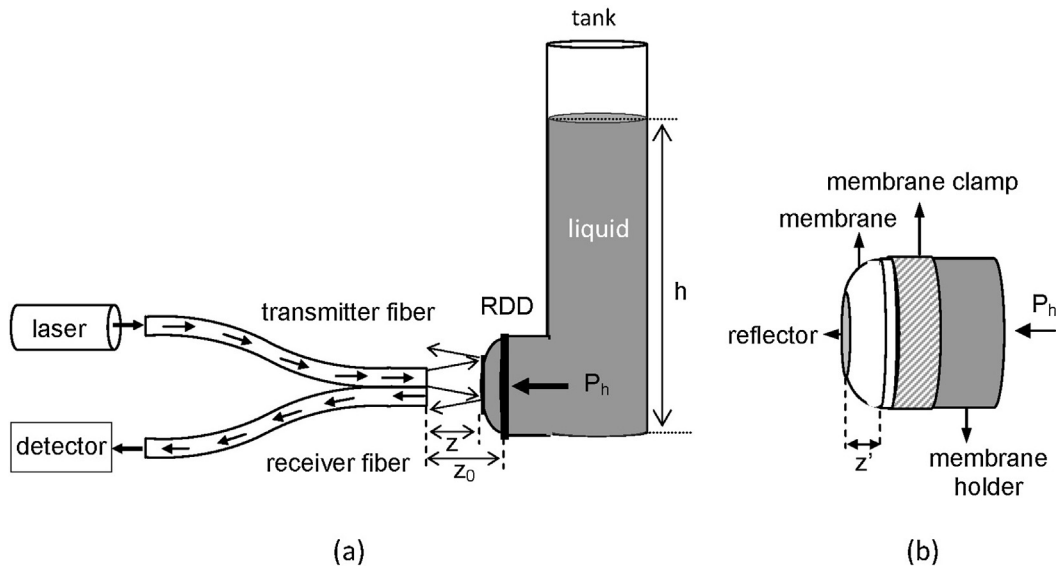


Fig. 1. The design of liquid level sensors using a pair bundle probe.

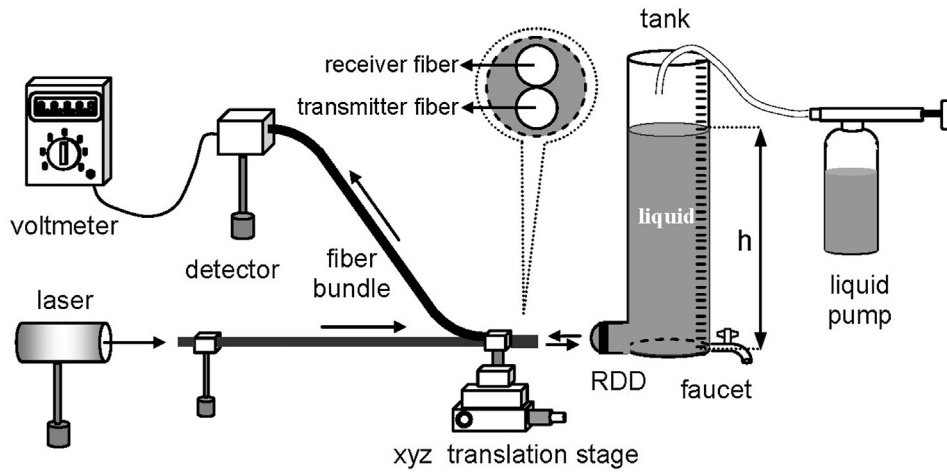


Fig. 2. Experimental set-up of liquid level sensor using a pair bundle probe.

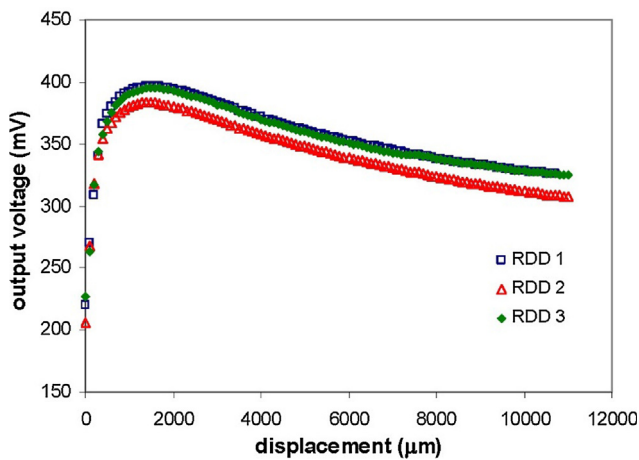


Fig. 3. The probe characteristic curve shifts to the reflector for all RDD used in the experiment.

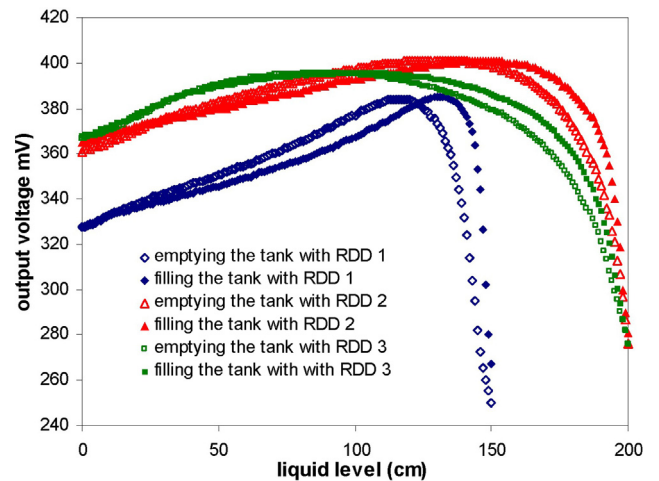


Fig. 4. Dynamic range (V versus h) for all RDD as result of scanning liquid level for to process of emptying and filling the tank.

**Table 1**  
Range of front slope and back slope are from liquid level scanning.

Area	RDD 1		RDD 2		RDD 3	
	Emptying	Filling	Emptying	Filling	Emptying	Filling
Range of front slope (cm)	0–116	0–131	0–130	0–146	0–90	0–104
Range of back slope (cm)	117–150	132–150	131–200	147–200	91–200	105–200

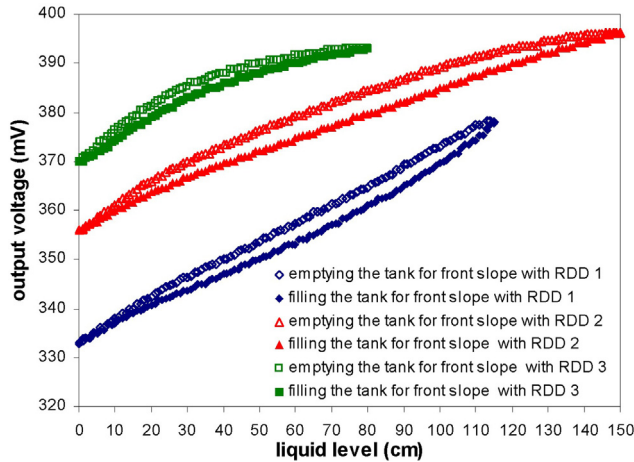


Fig. 5. Front slope curve of the liquid level sensor.

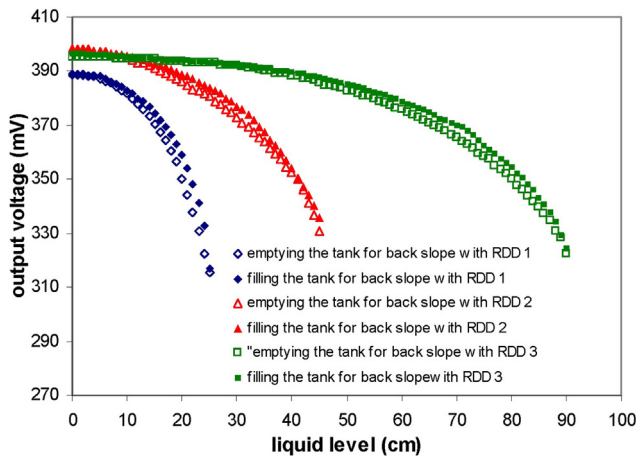


Fig. 6. Back slope curve of the liquid level sensor.

The detection principle of liquid level can be explained as follow: the light output of the transmitter fiber will be reflected by the reflector and received by the receiver fiber. The reflector will be shifting due to change in liquid level, as a result, the distance between the reflector toward the end of the fiber bundle that acts as a sensor probe ( $z$ ) also will be changed. This change can be detected by the intensity of light received by the receiver fiber that is measured on optical detectors. Thus, the liquid level is detected through changes in light intensity that are measured on optical detectors (in this case changes the output voltage detectors).

The relationship between the output voltage ( $V$ ) with displacement of reflector against the probe ( $z$ ), in the area close to the probe ( $z$  of about 1.7 mm) produces the front slope, and the rest produces the back

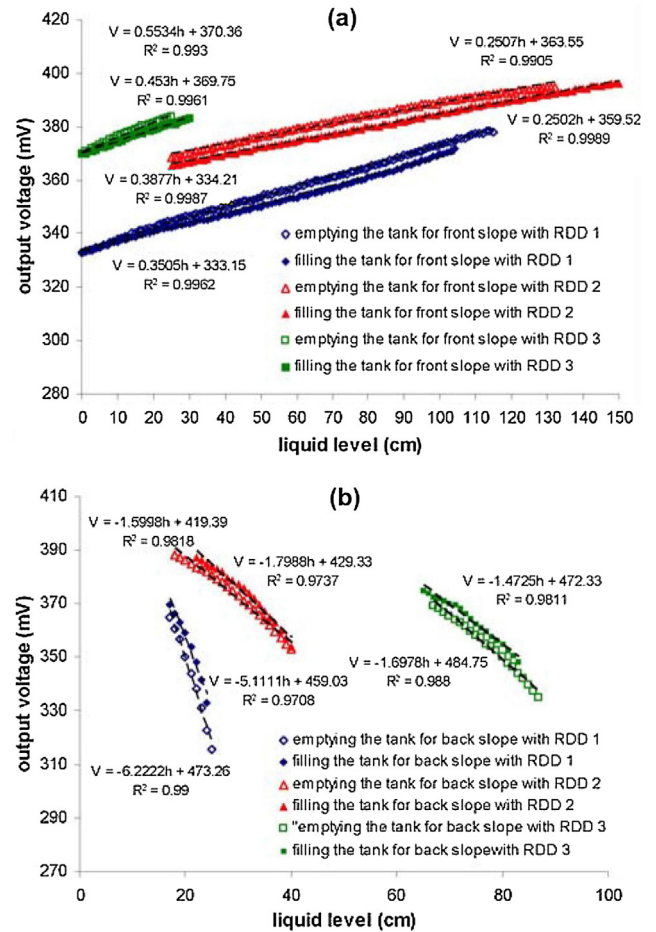


Fig. 7. Linear region of (a) front slope and (b) back slope.

slope [14]. Thus, the initial position of the probe against the reflector while the tank is empty ( $z_0$ ) will determine the characteristics of the sensor. For example, selected  $z_0$  as far as the range of front slope ( $z_0 = 1.7$  mm), then the dynamic range of the sensor has only one slope. If selected  $z_0 > 1.7$  mm and range of liquids level being detected produces displacement in reflector more than 1.7 mm, then the dynamic range of the sensor will produce two slopes (front slope and back slope). Therefore, the position of the  $z_0$  will determine the range of the sensor.

### 3. Experiment

Schematic diagram of the experiment is shown in Fig. 2. The experimental set-up consists of a laser semiconductor (with 630 nm wavelength and a 10-mW power output), silicon photodetector (818 SL), a pair bundle probes (from plastic material with 1 mm diameter and 2 m length) as a sensor probe, voltmeter (digital multimeter), xyz translation stage used to shift the probe sensor, manual liquid pump is used to pump liquid into the tank, cylindrical scaled water tank which is made of glass (with a diameter of 6 cm and 200 cm in length). In the bottom of the water tank, there are a faucet that is used for emptying the tank and reflector displacement device (RDD) consist of reflector which is made of aluminum (with 10 mm in diameter and thickness 0.20 mm), membrane (nitrile polymer) with 0.08 mm thickness (the elastic modulus is not known), and cylindrical membrane holder which is made of brass with 18 mm outer diameter and inner diameter of 15 mm. Reflector is attached to membrane using epoxy glue and membrane itself behaves like a spring. Three types of RDD used in this experiment i.e. RDD 1, RDD 2, and RDD 3 each consisting of 1, 2, and 3 layers membrane. In this experiment, the liquid used is water.

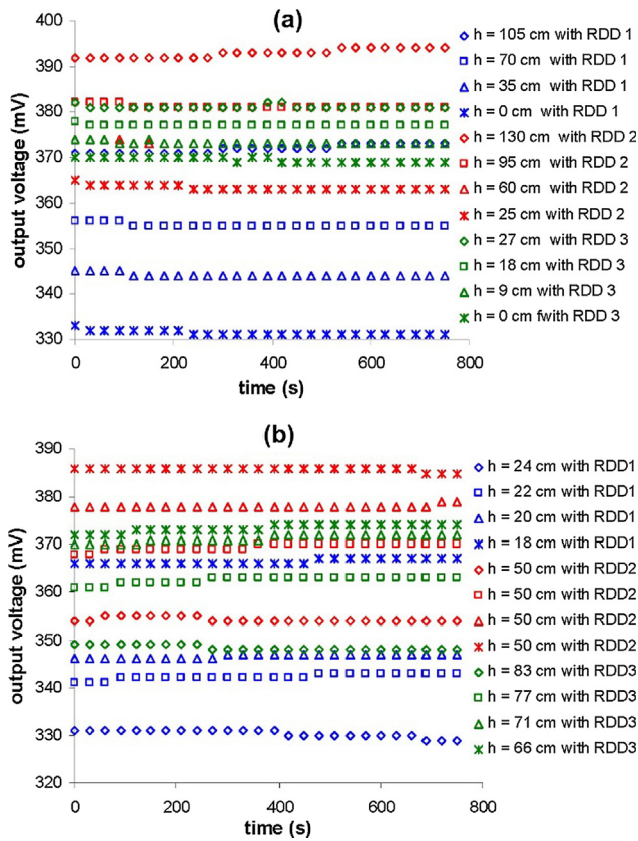


Fig. 8. Sensor stability curve for the area of (a) front slope and (b) back slope.

The first step of the experiment is to characterize the displacement of sensor probe against the reflector. The data were taken by placing a sensor probe located at the center and coincide with reflector RDD 1 (1 membrane layers) when the tank is empty. The recording of output voltage performed each probe shifted backward of 100 mm. Probe shifting was done using xyz translation stage. The second step is to characterize the liquid level sensor on the emptying process of the tank. The second step begins by filling the tank with liquid as high as 150 cm, then place the probe coincide with reflectors RDD 1 ( $z = 0$  mm). The liquid level limit was selected at 150 cm due to the maximum ability of 1 layer membrane to withstand hydrostatic pressure (liquid level more than 150 cm can deform 1 membrane layer). Furthermore, the recording of output voltage is performed every liquid level is lowered by 1 cm. After tank is empty, experiment proceeds to third step i.e. characterization of sensors when filling the tank with liquid. The third step is carried out by means of filling the tank with liquid using pumps. Each increase of 1 cm liquid level, recording of output voltage detector is performed. The recording was performed until the maximum level of the liquid in the tank is the same as the emptying process. The procedure is repeated three times. The procedure then repeated for RDD 2 (2 layers membrane) and RDD 3 (3 layers membrane). Because RDD 2 ability to withstand hydrostatic pressure is better than RDD 1, then the maximum level of the liquid used in the experiment for RDD 2 and RDD 3 is 200 cm.

The second and third step is scanning the liquid level, it was done to get the dynamic range of the relationship between the output voltage against the liquid level. Due to the displacement of the reflectors exceeded 1.7 mm, then the dynamic range has front slope and back slope. So, the front slope and back slope will be selected from the second and third step results. The fourth step is characterization of liquid level sensor respectively on the front slope and back slope. The final step is to test the stability of the sensor. The test was performed by measuring the output voltage in a span of 30 s over the 750 s. Stability test conducted

on the working area of the sensor range which is divided into four-point liquid level.

#### 4. Result and discussion

The characteristics of the probe displacement against all reflector RDD can be known through a voltage output as a function of the probe displacement. The results are shown by the curve in Fig. 3. From Fig. 3, it appears that the characteristics of the probe displacement against the reflector for all RDD are almost the same. This means that the reflector coincides on all RDD is almost identical. The curve in Fig. 3 has front slope on the displacement range of 1.5 mm and rest of the displacement range (9.5 mm) is the back slope. The occurrence of two slopes (front slope and back slope) on the dynamics range of displacement profile can be reviewed from sensor geometry. The sensor probe consists of two optical fibers adjacent to each other. An optical fiber acts as a transmitter and other optical fibers act as receivers. When the probe position coincides with the reflector, the output light from the transmitter fiber reflected off by the reflector, all goes back to the transmitter fiber. Thus no light enters the receiver fiber. The light received by the receiver fiber is read in the form of the output voltage of the detector. As the sensor probe begins to shift away from the reflector, a small portion of the reflected (reflected) light of the reflector begins to enter the receiver fiber. The larger the probe shift, the wider the reflected light beam of the reflector coming into the receiver fiber receiver. At a displacement of 1.5 mm, the width of the fiber receiver area is filled with reflective light beam from the reflector so that the maximum incoming light intensity (front slope) occurs. If the displacement is increased, then the reflected light beam from the reflector will expand. On the other hand, the fiber cross section area is fixed. Thus the intensity of light entering the receiver fiber decreases as the displacement is increased. The condition produces a back slope (1.5–11 mm shift).

The dynamic range of the sensor is known from scanning the liquid level sensor which produces an output voltage ( $V$ ) in response to changes in the liquid level ( $h$ ). For all RDD, the scanning results are shown in Fig. 4. Dynamic range for RDD 1 is 150 cm, while RDD 2 and RDD 3 have equivalent result i.e. 200 cm.

The curve in Fig. 4 shows that the front slope much more shallow than the back slope (inverted compared with the results of displacement characterization). This occurs because when the water level is maximum, the hydrostatic pressure also maximum so that the reflector position close to the sensor probe. The results also show that the dynamic range between filling and emptying process (hysteresis) is not the same. The difference is due to the nature of membrane relaxation after stress. The larger the membrane under pressure, the longer the relaxation time. It can be seen on the back slope of the curve in Fig. 4. The range of front slope and back slope for all RDD is shown in Table 1. The  $z_0$  value for RDD 1, RDD 2, and RDD 3 respectively are 7.7 mm, 4.77 mm, and 3.95 mm.

In dynamic range, there is a voltage output whose value is the same but for two different levels (located on the front slope and back slope). Therefore, the dynamic range is not the sensor range desired. To get the sensor range, we have conducted experiments with a limited range of liquid levels. Limit of level liquid used is based on the data in Table 1 to produce a front or back slope only. To get the front slope only,  $z_0$  is in the same position as when the liquid level scanning is performed and maximum limit of liquid level is the level indicated in Table 1. To get back slope only, the sensor probe is made coincident with the reflector when the water level has reached the limit of the range of local produce back slope. Data retrieval is performed three times.

The result of experiment to produce front slope of the sensor is shown in Fig. 5. From the curve in Fig. 5, it is known that the range of detection for RDD 1, RDD 2, and RDD 3 is respectively 115 cm, 150 cm, and 80 cm. The distance between the reflector to the probe ( $z$ ) of the at the maximum level for RDD 1, RDD 2, and RDD 3 is respectively 1.7 mm, 0.8 mm, and 1.5 mm. The average difference of output voltage

**Table 2**  
Characteristics of the liquid level sensor using a pair bundle probe.

Parameter	Front slope						Back slope					
	RDD 1		RDD 2		RDD 3		RDD 1		RDD 2		RDD 3	
	Emptying	Filling	Emptying	Filling	Emptying	Filling	Emptying	Filling	Emptying	Filling	Emptying	Filling
Sensor range (cm)	115	115	150	150	80	80	25	25	45	45	90	90
Linear region (cm)	0–115	0–104	25–132	25–150	0–25	0–30	17–25	17–24	18–40	22–40	67–87	65–83
Sensitivity (mV/cm)	0.39	0.35	0.25	0.25	0.55	0.45	6.22	5.11	1.6	1.8	1.7	1.47
Resolution (cm)	1.4	1.5	2.1	2.1	0.6	0.8	0.1	0.1	0.3	0.2	0.4	0.5

**Table 3**  
The comparison of performance between optical level sensors.

No.	Method	Sensor range (m)	Linear region (m)	Resolution (cm)	Ref.
1.	Fiber Bragg Grating	0.36	0.4	6	[1]
2.	Tapered chirped fiber grating	0.05	0.05	–	[2]
3.	Long-period Fiber Bragg Grating	1	–	10	[3]
4.	fiber interferometer using PCF	0.05	0.05	0.5	[4]
5.	Fiber optic-prism	0.014	–	0.1	[7]
6.	Plastic optical fiber polished	2.7 (discontinue)	–	–	[9]
7.	One output port fiber coupler	1.8	0.4	0.6	[10]
8.	Two output port fiber coupler	1	0.7	0.4	[11]
9.	Opto-fluidic	0.75	–	1.7	[12]
10.	Optical signal broadcasting	2	–	–	[13]
11.	A pair bundle probe (our paper)	1.15	1.1	1.4	–

at the same level for the process of filling and emptying for RDD 1, RDD 2, and RDD 3 is respectively 0.8%, 0.85%, and 0.40%. The largest measurement errors on RDD 1, RDD 2, and RDD 3 respectively are 0.9 mV (0.4%), 1 mV (0.25%), and 0.57, mV (0.15%). Apparently, the thicker the membrane, the smaller the measurement error.

For the back slope, the result is shown by the curves in Fig. 6. The average difference of output voltage at the same level for process of filling and emptying for RDD 1, RDD 2, and RDD 3 is respectively 0.8%, 0.6%, and 0.4%. The largest measurement errors on RDD 1, RDD 2, and RDD 3 respectively are 0.7 mV (0.3%), 0.58 mV (0.16%), and 0.57, mV (0.15%). The  $z_0$  value for RDD 1, RDD 2, and RDD 3 respectively are 5.53 mm, 2.7 mm, and 2.45 mm.

The back slope curve in Fig. 6, has a smaller slope than the curves in Fig. 4. This occurs because of the elasticity of the membrane decreases when the membrane gets smaller hydrostatic pressure so that the membrane displacement range depends on the magnitude of the hydrostatic pressure (liquid level) and not on the range of liquid level. That means reflector displacement is not linear against the hydrostatic pressure.

The linear region which is the working area of the sensor for front and back slope is shown in Fig. 7. The lowest level of linearity for the region is 99.5% for front slope and 98.5% for back slope. The slope in the linear region is the value of sensor sensitivity. The sensitivity of the sensor in the front slope area is smaller than the area of the back slope, but sensor range of front slope is a much larger than the back slope, except for the RDD 3. This happens due to limited level of the tank used in this experiment. In our opinion, dynamic range of sensor using RDD 3 could be even greater because membrane of RDD 3 is thicker than RDD 1 and RDD 2 so that it able to withstand the water pressure with an altitude higher than 200 cm.

Sensor stability test performed by selecting four points of the water level in the range of the sensor linear region. The results are shown in the curve of Fig. 8(a) and (b) respectively for the linear front slope and back slope. The largest standard deviation value in the linear region of front slope of RDD 1, RDD 2, and RDD 3 respectively is 0.54 mV, 0.54 mV, and 0.35 mV. While on the linear region of back slope, the largest standard deviation value for RDD 1, RDD 2, and RDD 3 respectively is 0.59 mV, 0.42 mV, and 0.68 mV. From these results, it can

be concluded that the stability of the sensor is good. The largest standard deviation value if divided by the value of the sensitivity of the sensor value will be the resolution of the sensor.

The sensor performance can be known through parameters such as sensor range, the range of the linear region, sensitivity, and resolution. Overall, the performance of the sensor both for front slope area and the back slope area is shown in Table 2. Based on the value of the parameters in Table 2, it is known that the best sensor performance in our opinion is a sensor that uses RDD 1 on the front slope area. The reason is because the working area of the sensor (linear region) starts from 0 cm. Although its range is smaller than the sensor using RDD 2, but the sensitivity and the resolution are better. For sensors using RDD 3, the actual characteristic cannot be observed due to the limited level of the tank used in the experiments. For sensors with a range of back slope area, although the sensitivity and resolution far better than the sensors with a range of front slope area, but the range and the area of work is lower. Excluding the parameter values for the use of RDD 3, the thicker the membrane is used, the larger the range and linear region sensors (the mean value between emptying and filling) are generated. Conversely, the thinner the membrane is used, the greater the membrane elasticity. Increase in membrane elasticity causes increase in sensor sensitivity. The impact of increase in sensitivity of the sensor is the smaller the value of the sensor resolution. This occurs due to the proposed sensor mechanism uses the hydrostatic pressure principle to detect the level of the liquid. However, each sensor either front slope or back slope can be used in accordance with needs, not only to detect the water but can also be used for gasoline [10,11]

The performance of the liquid level sensor using the optical fiber as a whole is shown in Table 3. Methods 1–4 is based on wavelength modulation. Methods 5–8 and 11 are based on intensity modulation. Methods 9 and 10 use opto-fluidic and Optical signal broadcasting respectively. Methods 7, 8, and 11 use the same working principle with our sensor that is based on optical fiber displacement sensors by utilizing hydrostatic pressure. When compared to results in methods 7 and 8, it appears that the working area of the sensor in our experiment is larger.

## 5. Conclusions

A pair bundle probes can be applied as a liquid level sensor based on displacement sensor. Utilization of hydrostatic pressure changes due to changes in liquid levels to shift the reflector is the basic working mechanism of the sensor. The experimental results show the use of 1 layer membrane as reflector displacement device produces the best performance sensor. Sensor range, working area (linear region), sensitivity, and resolution of the sensor with 1 layer membrane respectively are 115 cm, 110 cm, 0.37 mV/cm, and 1.45 cm.

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